1.9600 only 2208 18.8200 1045, 1413

3/135/60/000/010/017/018/XX

A006/A001

AUTHOR:

Navrotskiy, D. I., Candidate of Technical Sciences

TITLE:

Distribution of Stresses Between Transverse Seams

PERIODICAL: Svarochmoye proizvodstvo, 1960, No. 10, pp. 10-12

When calculating overlap weld joints with two transverse seams it is usually assumed that the stresses between the individual seams are uniformly distributed. This is, however, only correct in the case of joining parts of equal cross section loaded under certain conditions. If the rated cross section of the components to be welded are unequal or if the loading conditions are different, the aforementioned assumption may lead to serious errors. Methods are given to calculate weld joints with transverse seams permitting a more correct estimation of their operational conditions. Basic formulae are derived to determine the stresses in individual transverse seams for 3 different variants of weld joints and loading conditions:

1)  $P_1 = P_2 \left( 1 + \frac{\delta_2 - \delta_1}{\delta_1} \cdot \frac{ak}{ak + \delta_2} \right)$ 

Card 1/2

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S/135/60/000/010/G17/018/XX A006/A001

Distribution of Stresses Between Transverse Seams

where  $P_1$  and  $P_2$  are the stresses on the transverse seams, K is a constant coefficient whose value depends on the ratio of the weld joint dimensions;  $\theta_1$  and  $\theta_2$  are the dimensions of cross sections of the parts to be welded.

2) 
$$P_1 = P_2 \left( 1 + \frac{\delta_2 + \delta_1}{\delta_1} \cdot \frac{ak}{2} \right)$$

3)  $P_1 = P_2 \left[ 1 + \frac{2\delta_2}{\delta_1} \cdot \frac{ak}{ak + 2\delta_2} \right]$ 

Deformations in the seam zone are determined by dividing the weld joint into individual parts loaded by stresses which are applied to the dissected surfaces of the weld joints. The formulae obtained are analyzed and recommendations are given as to their use. There are 6 figures, 1 table and 2 references, 1 English and 1 Soviet.

ASSOCIATION: Leningradskiy politekhnicheskiy institut imeni M. I. Kalinina (Leningrad Polytechnic Institute imeni M. I. Kalinin)

Card 2/2

APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R0011362200

# PHASE I BOOK EXPLOITATION SOV/5500

# Navrotskiy, Dmitriy Ivanovich

Prochnost' svarnykh soyedineniy (Strength of Welded Joints) Moscow, Mashgiz, 1961. 174 p. 10,000 copies printed.

Reviewer: V.I. Kryzhanovskiy, Candidate of Technical Sciences; Ed.:
V.M. Savel'yev, Candidate of Technical Sciences; Ed. of Publishing House:
N.Z. Simonovskiy; Tech. Ed.: O.V. Speranskaya; Managing Ed. for Literature on the Design and Operation of Machines (Leningrad Department, Mashgiz):
F.I. Fetis rugineer.

PURPOSE: This L. . . Intended for technical personnel concerned with the design and manufacture of welded structures. It may also be used by students at schools of higher technical education and tekhnikums.

COVERAGE: Characteristics of welded joints are presented and their special features and advantages outlined. Attention is given to a consideration of the strength of welded joints under various operating conditions, methods of calculating the strength and endurance of welded joints, and examples of the use of welded joints in various weldments. No personalities are mentioned. There are 45 references: 42 Soviet, and 1 English.

18.8200

S/758/61/000/006/002/002

AUTHORS: Navrotskiy, D.I., Savel'yev, V.N., Candidates of Technical Sciences,

Chizhevskiy, S. V., Engineer.

The strength of welded joints of the aluminum allow AMr-6 (AMg-6). TITLE:

Leningrad. Nauchno-issledovateľskiy institut mostov. Sbornik trudov, SOURCE: no. 6, 1961. Soyedineniya elementov konstruktsiy iz a.yuminyevykh

splavov. pp. 163-171.

The paper reports strength and endurance tests of the AlMg alloy AMg-6 and AMg-6T, made on specimens 10 and 16 mm thick. The basic finding is that the TEXT: alloy is significantly more susceptible to variable loads than low-carbon steel. In weldments of AMg-6 alloy the static strength is primarily determined by the strength of the heat-affected zone. In high-temperature-welded specimens the weldment strength was from 80.5 to 92% that of the parent metal. The vibrational strength of the weldment was affected even more severely: In corner-weld specimens it was reduced to 52 to 57%, in butt-welded joints to 84%. Local machining of a joint, to provide a faired transition from parent metal to weld, increases the vibrational strength of the weldment considerably. The specimens tested in this series comprised: (1) Plain sheets, (2) sheets with welded-on stiffening ribs (with and without machined smooth fairings from parent metal to weld); (3) Tee-jointed pieces (wit and without machining); and (4) butt joints. The stiffening ribs were welded by hand

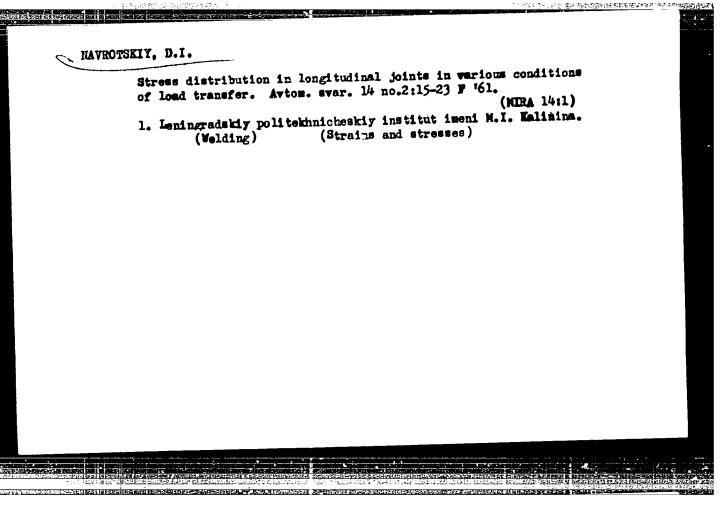
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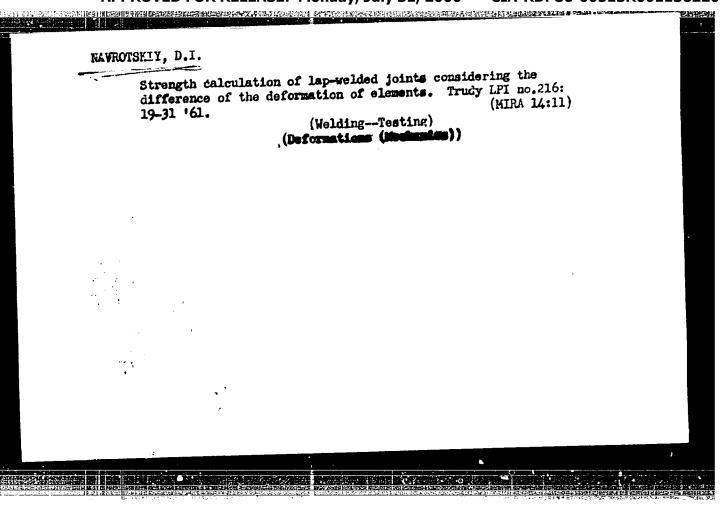
The strength of welded joints of the aluminum alloy... S/758/61/000/006/002/002

with argon-shielded arc welding, with a W electrode and a 4-mm diam AMg-6 welding rod, at an I of 300-340 a. The details of the single-pass consumable-electrode automatic welding of the unmachined Tee joints and the analogous three-pass procedure for the subsequently machined Tee joint is described, and cross-sectional views of the specimens are shown. Similarly welded consumable-electrode weldments with double-V butt joints were also prepared. Testing was done on the pulsation tester UUM-100 (TsDM-100). The mechanical properties of Gagarin specimens cut along and across the direction of rolling are shown in a full-page table. All mechanical characteristics are in excess of those required by Technical Specs TU15-57. The appreciable scatter of the test data is noted. Large-scale specimens were tested separately to investigate the effect of rolling surface scale and cladding. Tabulated data show that the yield limit of the parent metal on the flat specimens is somewhat higher than that of the Gagarin specimens, even though the tensile strength of both is practically the same. The static strength of specimen weldments of the various types is interpreted in terms of the heating undergone by them in the course of the welding process. The results of the vibrational tests are summarized in a table. The vibrational strength of the specimens is interpreted in terms of both the heating undergone and the notch effect represented by the change in cross-section from the unaffected parent metal to the weld. There are 4 figures and 3 tables. No references.

ASSOCIATION: None given.

Card 2/2





S/124/62/000/006/021/023 D234/D308

AUTHORS:

Navrotskiy, D. I. and Savel'yev, V. N.

TITLE:

Investigating the influence of residual stresses on the vibrational strength of specimens with small

stress concentration

PERIODICAL:

Referativnyy zhurnal, Mekhanika, no. 6, 1962, 56, abstract 6V494 (Tr. Leningr. politekhn. in-ta, 1961,

no. 216, 48-55)

TEXT: The authors tested three series of specimens cut from (51.3) steel for welded bridges and having round cuts on lateral edges, owing to which there was a non-uniform distribution of stresses in the design section. The effective concentration coefficient for the above specimens was \$\approx 1.2\$. All specimens were previously subjected to thermal treatment to remove possible residual stresses due to rolling or gas cutting. One series was tested in the initial state, the second series after heating their middle parts by gas heater in order to cause compression stresses

Card 1/2

Investigating the influence ...

S/124/62/000/006/021/0**23** D234/D308

on their lateral edges, the third series after stamping of their middle parts in order to cause tensile stresses on their lateral edges. The results of vibrational tests, re-calculated for a symmetrical cycle, showed an increase of durable strength by 4% in the specimens of the second series in comparison with the first and a decrease by 5.5% in the specimens of the third series. It is pointed out that all specimens of the second series started failing at the lateral edges in spite of the fact that the stresses in the middle of the design section amounted to approximately 2500 kg/cm² at the beginning of the tests and maintained a value of approximately 930 kg/cm² after first cycles. This is due to the fact that the negative influence of residual tensile stresses in the middle of the section was fully compensated by mechanical characteristics of the specimen's metal, increased owing to hardening. /Abstracter's note: Complete translation. /

Card 2/2

16764-63

EWP(k)/EWP(q)/EWT(m)/BDS

AFFIC/ASD Pf-4 JD/HJ 3/124/63/000/004/062/06

AUTHOR:

Navrotskiy D

TITLE:

A study of the influence of residual stresses on vibration strength in

elements with sharp cuts

PERIODICAL: Referativnyy zhurnal, Mekhanika, no. 4, 1963, 63, abstract 4V524 (Sb. Proyektir. i prochnost' svarn. konstruktsiy. M. -L, 1959, 172-184)

TEXT: The authors present the results of a test of the vibra-edgss, under the following initial conditions: condition at start; condition following heating of the median of the width of the sample to obtain stretching stresses at the root of the cute; following preliminary stretching which resulted in compression stresses and cold hardening of the metal at the root of the cuts and size in an increase in the radius of the cut; following heating of the edges at the points cf cut, this resulting in stretching stress within the cuts. The set of samples was subjected to thermal processing, following which it underwent a test for vibration load. To exclude the influence of thermal processing on the properties of the basic metal, the sheets from which the samples were prepared were themselves subjected to thermal processing, so that the subsequent thermal operation could vary only those properties and stresses which were brought about by the heating, plastic compression or stretching of the samples. The character of the distribution and the magnitude of the residual stresses Card 1/2

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A study of .....

created by the different processing of the samples were determined by the method of section by readings of a resistemeter. The vibration strength of the samples with residual compression stresses turned out to be higher than that of the initial (without residual stresses); that of samples with residual stretching stresses — lower. The stretching of samples increased their vibration strength. Repeated thermal processing brought the samples into a condition in which their vibration strength was about the same as that of the initial, except for samples subjected to stretching. The vibration strength of these samples, as the result of repeated thermal processing, was somewhat lowered (by cold hardening and compression stresses), but nevertheless remained harder than in the initial state, since the increased radius of cut was perserved following the repeated heating.

The studies made enabled the investigators to make a more precise estimation of the influence of stresses, plastic deformations, bold hardening and variations in the sharpness of cut, on the vibration strength of samples. N. O. Okerblom.

[Abstracter's note: Complete translation.]

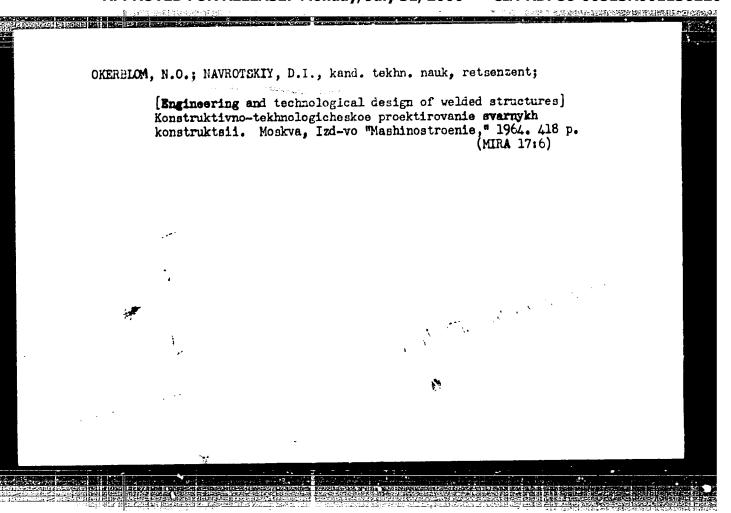
Card 2/2

SAVEL'YEV, Vladimir Nikolayevich, kand. tekhn. nauk; CHIZHEVSKIY,
Svyatoslav Valeriyevich, inzh.; NAVROTEKIY, Dmitriy—
Ivanovich, kand. tekhn. nauk; KAZDUY, F.I., red.;

[Technology of welding processes and the strength of welded joints of aluminum-magnesium alloys] Tekhnologiia svarki i prochmont' svarnykh soedinenii iz aliuminievo-magnievykh splavov. Leningrad, 1963. 28 p. (Leningradskii dom nauchno-tekhnicheskoi propagandy. Ohnen peredovym opytom. Seriia:
Svarka, paika i rezka metallov, no.5)

(MIRA 17:4)

# NAVROTSKIY, D.I. Stress concentration in welded joints made by transverse seam welding. Trudy IPI no.229:16-24 '63. (MIRA 17:9)

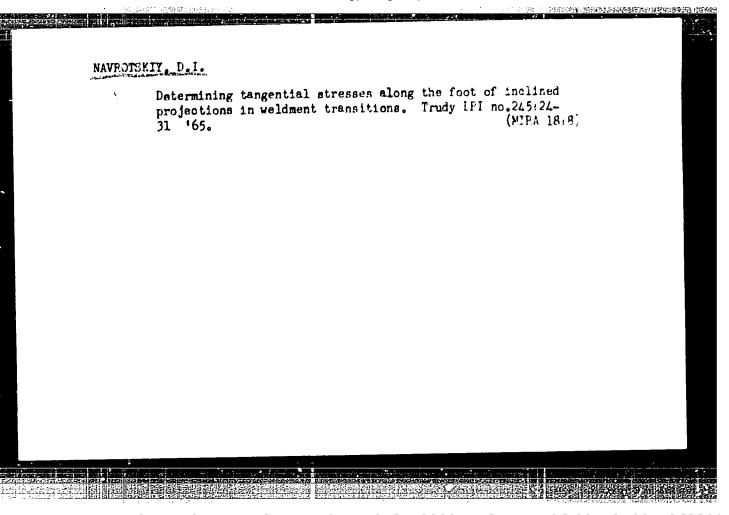


### "APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R001136220

NAVROTSKIY, D.I., kand. tekhn. nauk

Methods of calculating welded joints, taking into account concentrations of stresses. [Trudy]LMZ no.11:39-51 \*64. (MIRA 17:12)



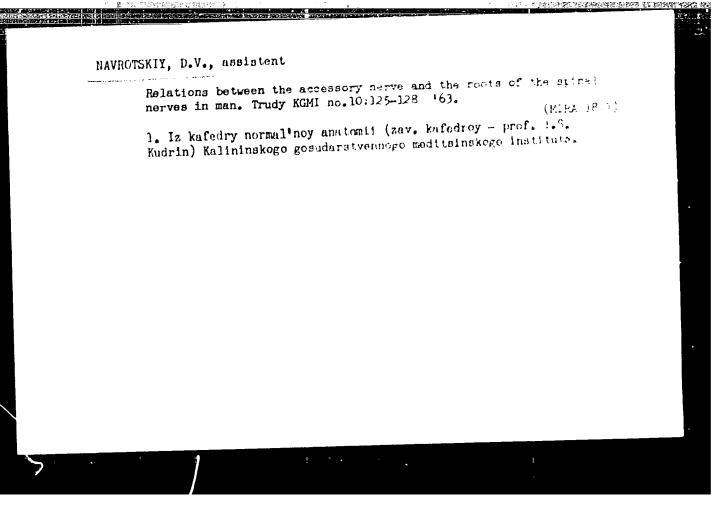
L 32848-66 ENT(m)/ENP(x)/T/ENP(t)/ETI/ENP(L) JD/HM ACC NR. AR6000443 . SCURCE CODE: UR/0137/65/000/009/	E011/E011
ACC NR, ARGOOGHAS	38
AUTH.A: Navrotskiy, D. I.	B
TITLE: Determining local elastic deformations in spot-welded joints	
SOURCE: Ref. zh. Metallurgiya, Abs. 9871	-
TOPIC TAGS: metal welding, spot welding, elastic deformation	
ABSTRACT: Equations are given for use in the solution of statistics problems connected with the calculation of spot-welded joints and as use of spot-welded joints with more than three spots in a linear round because a greater number of spot welds does not contribute to the power of the joint. This is explained by the fact that the middle power of the joint.	e is not practi- he supportive points carry the neressed rather
least load. It is recommended that the dimeter of spot than their number in linear row in order to increase the supportive welded joints. V. Fomenko. [Translation]	power of spot-
About hely mether in linear row in other to the	power of spot-
than their number in linear row in older to restrict the welded joints. V. Fomenko. [Translation]  SUB CODE: 11/ SUBM DATE: none	power of spot-
than their number in linear row in older to receive welded joints. V. Fomenko. [Translation]	power of spot-
than their number in linear row in older to reduce welded joints. V. Fomenko. [Translation]  SUB CODE: 11/ SUBM DATE: none.	power of spot-

BUDYACHEVSKIY, A.T.; VFKSLFRCHIK, R.A.; MOPEVA, A.G.; MAVROTSKIY, D.S.;

NOVINSKAYA, I.W.

Emergency aid in acute percently insufficiency. Kardiologila
5 no.1:87-88 Ja-F 165. (MIPA 18:9)

1. TSentral'maya stantsiya skoroy meditainskoy (glavny, vrach
N.K. Gavrilova; nauchnyy rukovoditel' - prof. C.V. Shestakov),
g. Kuybyshev.



### MAYROTSKIY, P.I.

Outlieosynthesis combined with bone grafiting of a preserved rib for treating a nonknitting fracture of the mandible complicated by chronic esteemyelitis. Stematologia 36 no.3:34-35 Ky-Je '57. (NIPA 10:9)

1. Is kliniki chalyustno-litsevoy khirurgii i stomatologii Voyenno-maditsinekoy ordena Lenina akademii imeni S.M.Kirove (JAW3-SURGERY) (BONE GRAFTING) (OSTROMYELITIS)

NAVROTS: I. G. A.

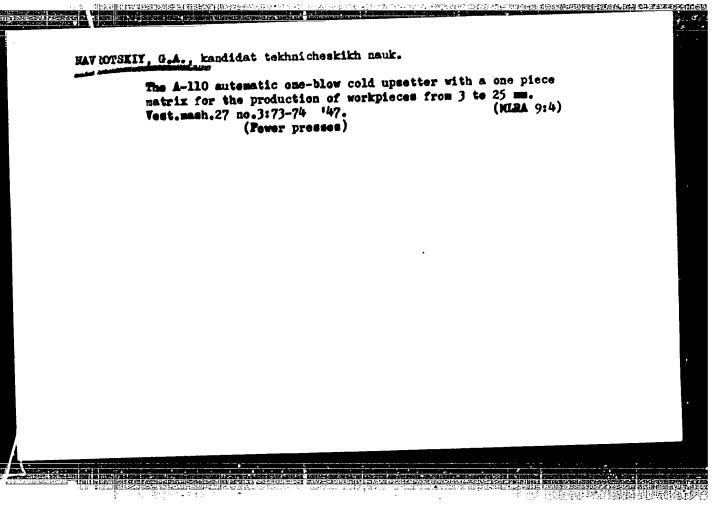
Kholodnovysadochnye avtomaty; konstruktsiia i raschet. Moskva, Mashgiz, 1944.

131 p.

(Automatic upsetting machines; design and calculation.)

DLC: Unclass.

SO: Manufacturing and Mechanical Engineering in the Soviet Union, Library of Congress, 1953.



HAVROTSKIY, G. A.

Parovozdushnyi 1000-kg kovochnyi molot. (Vestn. Mash., 1948, no. 2, p. 49-50)

Refers to Voronezh Kalinin machine-building plant.

(1000-kg. air-steam forging hammer.)

DLC: TN4.V4

SO: Manufacturing and Mechanical Engineering in the Soviet Union, Library of Congress, 1953.

NAVROISKIY, G. A.

Vysadochnye i obreznye pressy-avtomaty. Moskva, Mashgiz, 1949. 253 p. illus.

"Nastoiashchaia rabota iavliaetsia prodolzheniem knigi avtora 'Kholodnovysadochnye avtomaty.'

Bibliography: p. 250-(251).

(Automatic upsetting and trimming presses.)

DLC: TJ1450.N3

SO: Manufacturing and Mechanical Engineering in the Soviet Union, Library of Congress, 1953.

HAVROTSEIY, G.A., kandidat tekhnicheskikh nauk. Economising metals by the introduction of cold upsetting. (In: Byshkov, D.A., ed. Economia metallov v kusnechno-shtampovechnom (MERA 7:1) proisvodatve. Noskva, 1953. p.176-193.) (Forging) (Punching machinery)

CIA-RDP86-00513R0011362200

APPROVED FOR RELEASE: Monday, July 31, 2000

MAVROTERTY, G. A. USSR/Engineering - Cold forging 1/1 Pub. 128 - 9/32 Card Navrotskiy, G. A. Authors Problem of determining the magnitude of stress during cold forging Title : Vest. mash. 34/7, 30 - 34, July 1954 Periodical Experiments were conducted to determine the magnitude of stress during Abstract cold forging. On the bases of these experiments, the author was able to compile a formula for determining mechanical deformations, and the magnitude of stress. The cold forging of rivets was performed by means of TsNIITMSh-4, Amsler-50, 82VA, and type 70, machines. Four references. Illustration; drawing; diagram; graphs; table. Institution Submitted

HAVROTSKIY, Georgiy, Aleksandrovich, kandidat tekhnicheskikh nauk; RUSKEVICH, Rikhail Leoht Yevich; SHIFRIH, S.M., nauchnyy redaktor; RUKOVA, I.V., redaktor; RGGERT, A.P., tekhnicheskiy redaktor [Automatic cold upsetting machinery] Kholodnovysadochnye avtomaty.

[Automatic cold upsetting machinery] Eholodnovysadochnye avtomaty.

Moskva, Vses. uchebno-pedagog. isd-vo Trudreservisdat, 1956. 68 p.

(Metal working machinery)

(MLRA 9:7)

PHASE I BOOK EXPLOITATION SOV/1422

Navrotskiy, Georgiy Aleksandrovich, Candidate of Technical Sciences,

Pressy-avtomaty dlya kholodnoy shtampovki (Automatic Presses for Cold Working) Moscow, Mashgiz, 1956. 350 p. 8,000 copies printed.

Ed.: I.S. Pobedin, Candidate of Technical Sciences; Ed. of Publishing House: V.A. Mezhova; Tech. Ed.: S.L. Shmel'kina; Managing Ed. for Literature on Heavy Machine Building (Mashgiz): S.Ya. Golovin, Engineer.

PURPOSE: The book is intended for the engineering staff of forging and stamping plants and may be useful to students in mechanical engineering vtuzes.

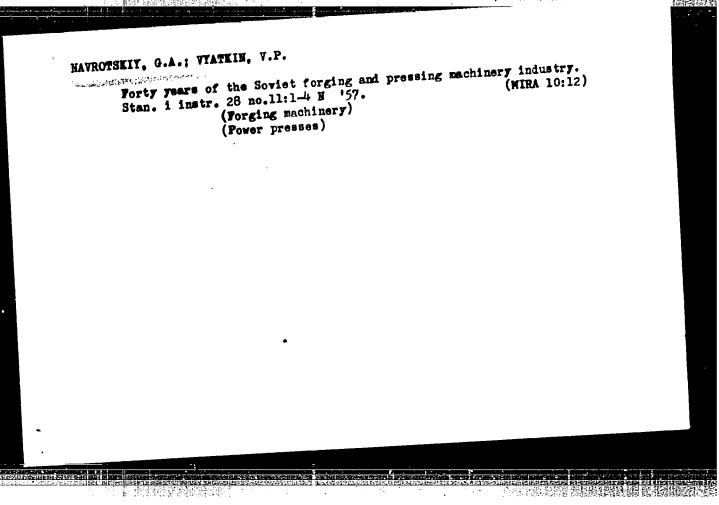
COVERAGE: The book presents a classification system for automatic forging and stamping presses, methods of kinematic and kinetostatic design for basic mechanisms, a description of constructions of commonly used types of automatic presses for stamping and die forging, and a description of universal automatic bending machines. The book uses investigations conducted by TaBKM (The Central Bureau for Building Card 1/5

# sov/1422 Forging and Pressing Machines) and other design bureaus, and by plants .Automatic Presses (Cont.) building and using machinery of this kind. This book is a continuation and development of books written earlier by the same author: Kholodno-vysadochnyye avtomaty (Automatic Machines for Cold-upsetting), Mashgiz, 1945; Vysadochnyye 1 obreznyye pressy-avtomaty, Mashgiz, 1949. The author used theoretical principles developed in the works of I.I. Avtobolevskiy, S.I. Artobolevskiy, G.A. Shaumyan, A.I. Zimin, A.I. Tselikov, S.I. Gubkin, A.D. Tomlenov, E.P. Unksov, L.A. Shofman, M.V. Storozhev. There are 42 references, all Soviet. 3 TABLE OF CONTENTS: PART I. DESIGN ELEMENTS OF BASIC MECHANISMS, AND GENERAL Foreword Classification and Principles for Operating Automatic 5 ch. 1. Presses Card 2/5

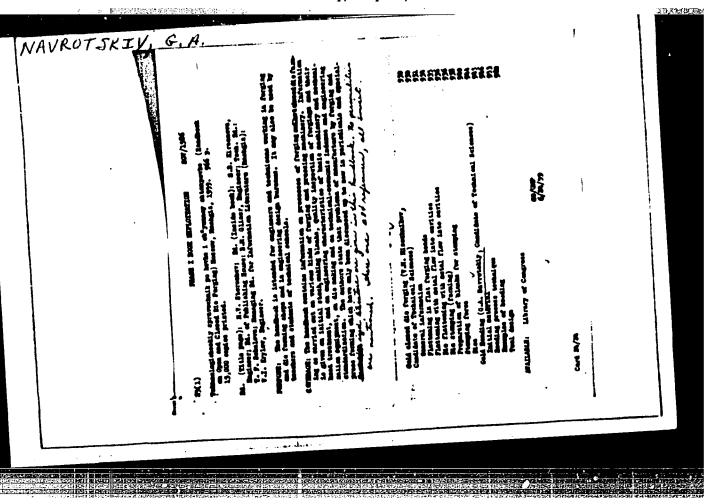
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S/028/60/000/011/003/007 B020/B058

AUTHORS:

Yegorov, N. A., Navrotskiy, G. A.

TITLE:

Grouping and Standardization in the Construction of Forging

Presses

PERIODICAL:

Standartizatsiya, 1960, No. 11, pp. 16-23

TEXT: The standardized units and parts assembled and tested before the assembly of the entire machine are the basis of forging presses. The various types of forging press units are schematically shown in Fig. 1. Fig. 2 shows a grouping scheme of forging press units, which shows more clearly the correlation between the various units and deals better with problems of standardization of units and parts. All units are divided into classes A (installations with translatory motion) and B (installations with rotary motion), which are subdivided into types I, II and III, IV. with rotary motion), which are subdivided into types I, II and III, IV. with consisting of individually assembled units mounted on a machine Units consisting of individually assembled units consisting of different frame belong to types I and IV. Each type of class A machines is machines belong to types II and IV. Each type of class A machines is divided into those with one and those with several crossheads; moreover, divided into those with one and divided into types. Some examples for the Card 1/3

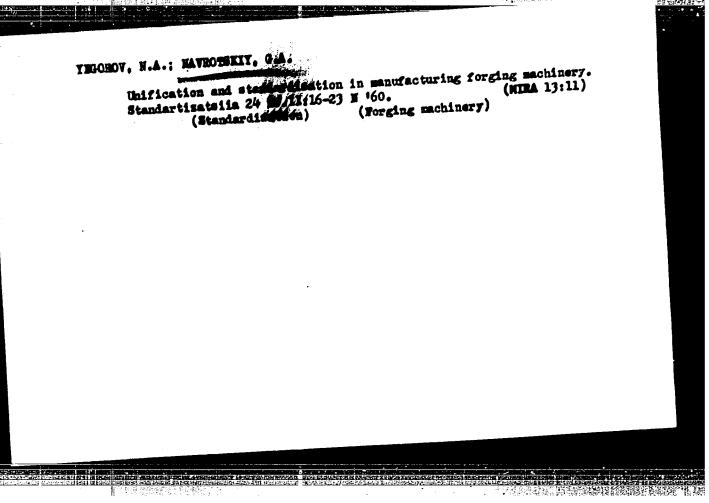
Grouping and Standardization in the Construction S/028/60/000/011/003/007 of Forging Presses

grouping of forging-press units are presented. Fig. 3 shows an open, inclined press unit from the British firm of Johns, Fig. 4 a 6-ton open hydraulic press unit from the firm of Denison, Fig. 5 the power head of a press unit from the firm of Clearing, mounted on various frames similar to metal machining units. Fig. 6 samples for the assembly of special presses using power heads from the firm of Clearing, Fig. 7 a single crank power head designed by the Tsentral'nyy byuro kuznechno-pressovogo mashinostroyeniya (Central Office for Forging-press Construction) (TsBKM), Figs. 8 and 9 examples for its mounting on presses of various types, and Fig. 10 a variant of using the same frame combined with mechanical and hydraulic power heads. Power heads with a capacity from 4 to 250 t (Table 1) enable the combination of 63 standard types of universal crank machines and 37 hydraulic machines. The average increase of the number of these highly important press parts which are most difficult to manufacture, amounts to 4 to 12 in series production. The simplification in the design of a 63-ton single-crank press unit is shown in Table 2. Fig. 11 shows that the number of joint parts for four types of single-crank presses amounts to about 70-75%. Fig. 12 shows that work expenditure for the open 63-ton presses, manufactured by the Taganrogskiy zavod kuznechnopressovogo oborudovaniya (Taganrog Plant for Forging-press Installations), Card 2/3

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Grouping and Standardization in th Construction S/028/60/000/011/003/00 of Forging Presses

can be reduced by using a joint power head. Finally, it is pointed out that the TeBKM and Eksperimental'nyy nauchno-issledovatel'skiy institut kuznechno-pressovogo mashinostroyeniya (Experimental Scientific Research kuznechno-pressovogo mashinostroyeniya in Scientific Research kuznechno-pressovogo mashinostroyeniya in Scientific Research kuznechno-pressovogo mashinostroyeniya (Experimental Scientific Research kuznechn



Whyrotskiy, (-.-)

PHASE I BOOK EIPLOITATION SON/5799

Unksov, Ye.P., Doctor of Technical Sciences, Professor, Ed.

Sovrementorye sostoyaniye kunnechno-shtempovochnogo proisvodstva (Present State of the Pressvorking of Metals) (Moscow) Nashgis, 1961. 434 p. 5000 copies printed.

Ed. of Publishing House: A.I. Sirotin; Tech. Ed.: B.I. Modol'; Managing Ed. for Literature on the Hot Working of Metals: S.Ta. Golovia, Engineer.

Title: Kunnechno-shtempovochnoye proisvodstvo v SSSR (The Prosvorking of Hetals Oirah (Saccash), L.D. Goliman, S.P. Granovskiy, N.B. Dobrinskiy, A.I. Zinia, Girah (Saccash), L.D. Goliman, S.P. Granovskiy, N.B. Mortynov, P.R. Hondon, S.L. Literature, A.I. Kagalovskiy, P.V. Lobachev, N. Martynov, P.R. Hondon, Y.A. Stocha, Yu.L. Sinin, G.A. Barvinskiy, Y.V. Mortynov, S. M. Scheglov, and L.A. Bhor-Reb Hastevenskiy, N.V. Tithonirov, Te.F. Unksov, N.Scheglov, and L.A. Bhornov.

Title: Kunntchno-shtempovochnoye proisvodstvo v ChSSR (The Pressvorking of Metals in the Usechoslovsk SR) by: S. Burda, F. Brazdil, F. Drastík, F. Zlatchlávsk Card 1/8

的情况的1965年1967年1975日本**经**的情况时间 36 801,5799 Present State of the (Cont.) Z. Kejval, V. Krauz, F. Kupka, F. Hajer, K. Marvan, J. Hordk, J. Odchnal, K. Paul, B. Scmmer, M. Honz, J. Castka, V. Sindeldr, and J. Sole; Eds.: A. Nejepsa end M. Vlk. PURPOSE: This book is intended for engineers and scientific personnel concerned with the pressworking of metals. COVERNOE: Published jointly by Mashgiz and SHTL, the book discusses the present state of the pressworking of metals in the USER and the Czechoslovak Socialist Republic. Chapters were written by both Soviet and Czechoslovak writers. Ro personalities are montioned. There are 129 references: 98 Soviet, 16 English, 8 German, 5 Czech, and 2 French. TABLE OF CONTENTS: PRESSMORKING IN THE USER Ch. I. The Characteristics of Forging Shops in USER Plants [A.I. Zimin and (h. II. Methods of Calculating the Pressure for Forging in the Pressvorking Card 2/8

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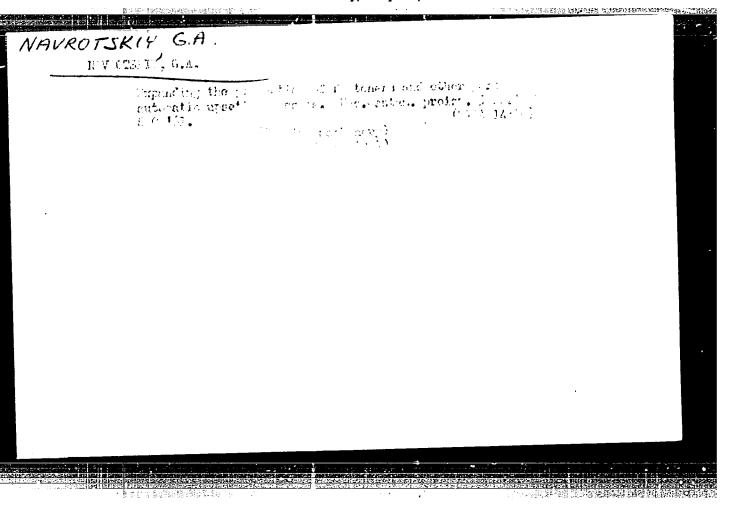
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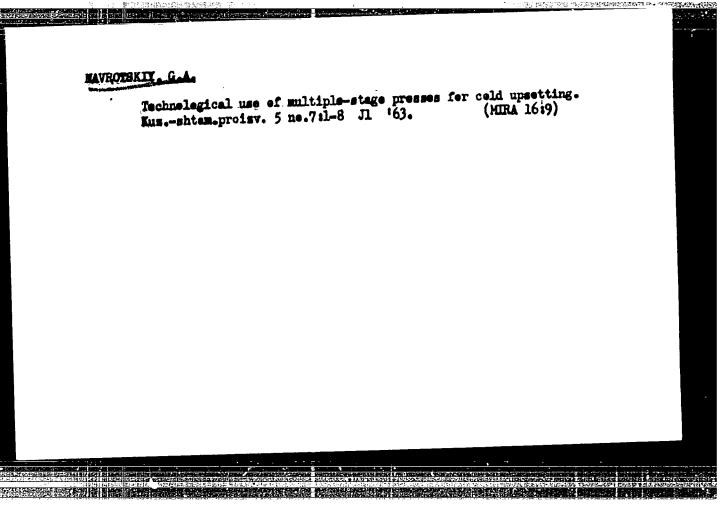
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POPOV, V.A., kand. tekim. nauk; MISOZHNIKOV, V.M., kand. tekim.
nauk, retsenzent; NAVROTSKII. G.A., kand. tekim. nauk,
retsenzent; GIMENTUK, Ye.A., inzh., red.

[Equipment for automated cold upsetting processes] Osnastka
avtomatizirovannogo kholodnovysadochmogo proizvodstva. Moskva, Mashinostroenie, 1965. 174 p. (MIRA 18:8)

HAVROTSKIY, G. Ye. (Engineer)

Compressors

Use of steam-jet compressors for heating. Za ekon. top. 9, No. 5, 1952

9. Monthly List of Russian Accessions, Library of Congress, August 1952 1953, Uncl.

Navnotskiy I.V.

AUTHORS:

Kurmanov, M.I., Navrotskiy, I.V.,

Yanushevskaya, Zh.F.

32-1-40/55

TITLE:

A Device for the Investigation of the Damping of Oscillations in Metals (Ustanovka dlya issledovaniya zatukhaniya kolebaniy

v metallakh).

PERIODICAL:

Zavodskava Laboratoriya, 1958, Vol. 24, Nr 1, pp. 101-103 (USSR)

ABSTRACT:

In this paper the construction of such a device is described and examples for the computation of the logarithmic damping decrement of oscillations are given. The principal part of this device consists of a firmly welded frame which is suspended from the ceiling by means of a rope. In the upper part of the frame there is a clamp, by means of which the sample is fastened, which has the form of a metal strip, and on which oscillations are measured. At the edge of the sample a magnet is mounted in a metal setting. Under the magnet, on a table, there is a coil with 600 windings. By means of a screw it is possible to adjust the distance between the magnet and the coil. By the micrometer screw the initial

Card 1/2

bend-through of the sample is fixed by the magnet. When switching

A Device for the Investigation of the Damping of Oscillations in Metals

32-1-40/55

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off the magnet the sample begins to oscillate; oscillations slowly die down while the current formed in the coil is led to the oscillograph, and a vibrographic recording is made. The logarithmic damping decrement is then computed according to the following

formula:  $\int = \frac{\ln 2}{n-1}$ 

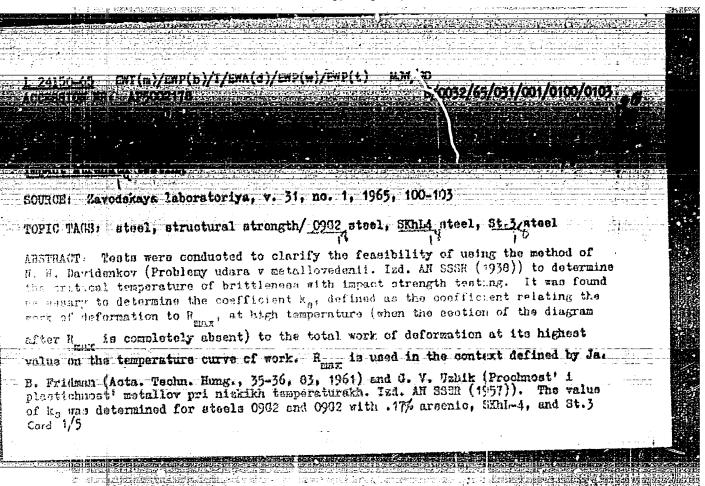
where n denotes the number of vibrations. There are 5 figures.

ASSOCIATION: Ukrainian Scientific Research Institute for Metals (Ukrainiskiy

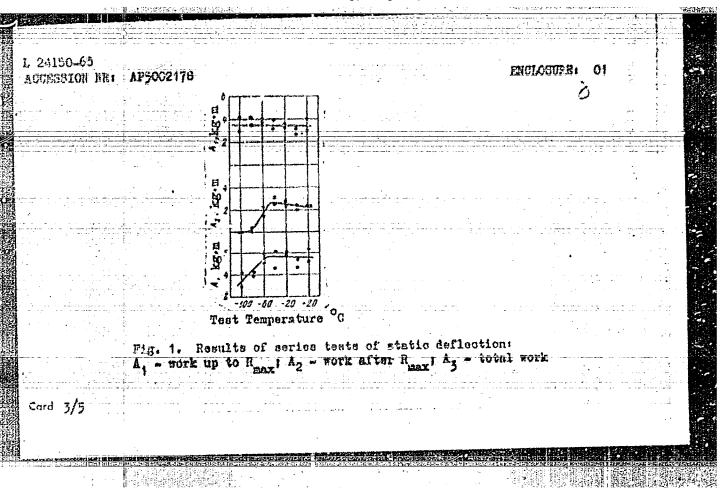
nauchno-issledovatel'skiy institut metallov).

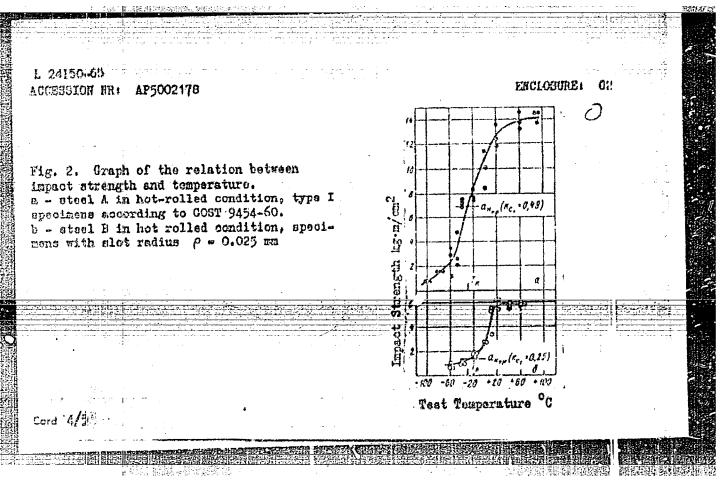
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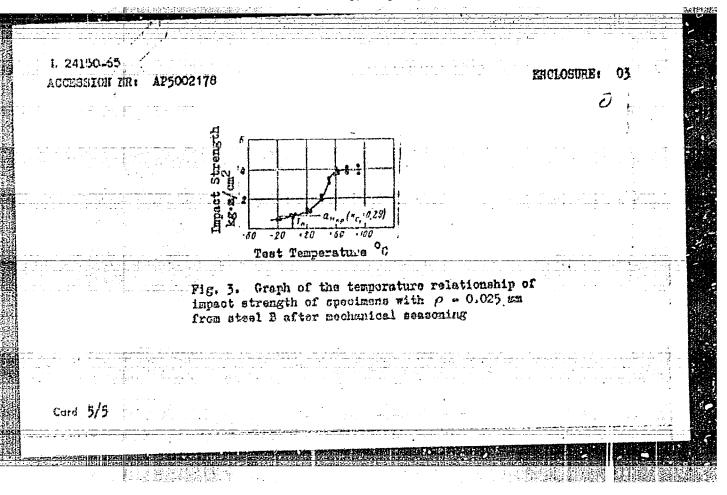
Card 2/2 1. Oscillations-Control systems



tested according to Davidenkov's methods. Several factories prepared the specimens, various shapes, sizes, and preparation procedures of which were used. Results of the plotted test measurements are shown in Figures 1, 2, and 3 on the Enclosures. Crig. and has: 3 figures and 3 tables.  ASSOCIATION: Ukrainskiy nauchno-issledovatelskiy institut metallov (Ukrainian			
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SOV/32-24-9-29/53

AUTHORS:

Tomenko, Yu. S., Navrotskiy, I. V., Volchek, F. R.

TITLE:

The Computation of Impact Energy in Multiple Impact Tests (Raschet energii udara pri ispytaniyakh na povtornyy udar)

PERIODICAL:

Zavodskaya Laboratoriya, 1958, Vol 24, Nr 9, pp 1122-1125 (USSR)

ABSTRACT:

The latest ram impact machine models for multiple impact tests DSVO 150) possess several construction details that have an essential influence on the impact energy. A diagram of the operation of the machine, and of the connection of an oscillograph MPO 2 is given. The oscillograph reveals the movement of the ram from the initial position to the impact. The operation of the machine is described, and the calculation methods by L. T. Timoshuk (Ref 1) is mentioned. From the analysis of the oscillograms it was found that, in principle, the machine may work in different ways, which fact is of significance for the computation of impact energy. There may be three different cases, a description of which is given. Graphs and calculation formulae are presented. The investigations of the operation of the ram at different spring tensions showed the separation factor of the roll from the ram to depend only on the clearance of the

Card 1/2

SOV/32-24-9-29/53

The Computation of Impact Energy in Multiple Impact Tests

spring, and not on the degree of its tension.
There are 4 figures and 1 reference, which is Soviet.

ASSOCIATION: Ukrainskiv nauchno-issledovatel'skiy institut metall:
(Ukrainan Scientifi: Institute of Metals)

Card 2/2

KURMANOV, M.I., kand.tekhn.nauk; MAVROTSKIT, I.V., insh.; FILIPPOVA,
T.F., insh.

Effect of arsenic on the properties of MicC steel (state
standard 6713-53). Trudy Ukr.nauch.-isel.inst.not. no.5;
187-200 '59. (MIRA 13:1)

(Steel--Testing) (Arsenic)

RAVROTSKIY, I.V., insh.; TOMEHKO, Yu.S., insh.; BRONINA N.Ye.; YES'KOV,
A.I.

Investigating the process of impact fatigue by a DSVO-150
testing machine. Trudy Ukr.nauch.-issl.inst.met. no.5:
287-301 '59. (MIRA 13:1)
(Metals--Fatigue) (Testing machines)

EVELUATION, M.I.; NAYROTSKIY, I.V.; TOMENKO, Yu.S.

Evaluation of the cold brittleness of structural sheet steel. Zav.

(MIRA 13:4)

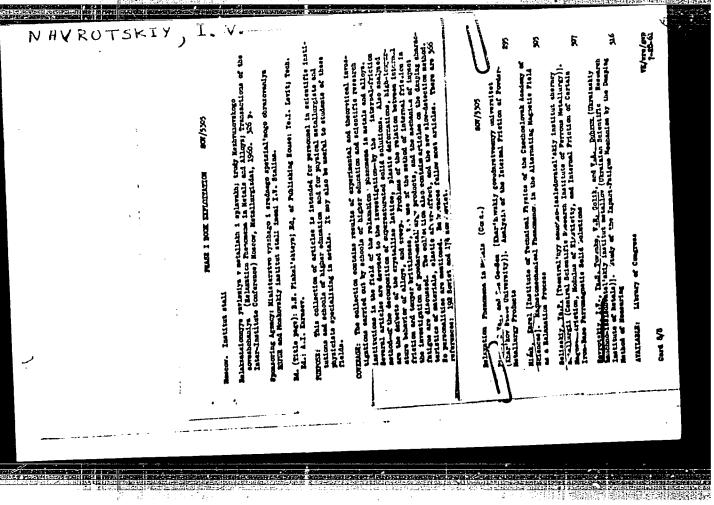
lab. no.11:1370-1372 '59.

1.Ukrainskiy nauchno-issledovatel'skiy institut metallov.

(Steel --Brittleness)

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AUTHORS:

Navrotskiy, I.V., Tomenko, Yu.S.

On the magnitude of maximal loading for brittle fracture TITLE:

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no.9, 1961, 38, abstract 9Zh232 ("Sb. tr. Ukr. n.-i. in-t, metallov", 1960, nc. 6, 206 - 216)

Investigations were carried out on Eucliberg specimens made of low-TEXT: alloy structural steels 10XCHA, 1CXTCHA, 15TAOT (1CYNEMD, 1CKNESHD, 15DMCT), low-carbon steel Mi6C and CT.3 (Mi6S and St.3) with As content C.18 and C.27%. The specimens were out out in the transverse direction to the rolling from sheets 12 mm thick. The value of the critical load at static rupture and at a blow on the stressed specimen was determined. Too experiments were carried out at 20,0, -20, -40 and -60°C. The maximum value of the static strongth of the metal under brittle fracture in the presence of a sufficiently rigid concentrator depends on the off-the-center position of the applied load, the level and orientation of the residual stresses and the gradient of the normal stresses over the specimen cross section. In the absence of these factors the brittle strength of the metal

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cannot be lower than the values of \$\delta\_g\$ in smooth symptomes. The nature of the variation in \$\delta\_b\$ as a function of temperature then head but correspond to the variation in the ductility properties.

M. Matveyeva

[Abstracter's note: Complete translation]

KURMANOV, M.I.; NAVROTSKIY, I.V.; TOMENKO, Yu.Sh.; DOERUSKINA, Zh.R.

Structural strength of certain high-resistance low-alloy steels. Trudy Ukr. nauch.-issl. inst. met. no.6:217-229 '60.

(Steel alloys-Testing)

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s/137/62/000/005/088/150 A006/A101

AUTHORS:

Navrotskiy, I. V., Tomenko, Yu. S.

TITLE:

The effect of elastic-energy storage upon the mechanical properties

of pipe steel

PERIODICAL: Referativnyy zhurnal, Metallurgiya, no. 5, 1962, 33, abstract 51188

("Sb. tr. Ukr. n.-1. in-t metallov", 1961, no. 7, 245 - 257)

The authors studied the mechanical properties of 19  $\Gamma$  (190), 16  $\Gamma$  2  $\Phi$   $\Gamma$ (16G2FT) and 16 F 2 (16G2) steel pipe specimens with different V content and pos-TEXT: sessing different elastic-energy stores in tensile and static bending tests. In a non-insulated system, an increase in the elastic-energy storage does not affect the mechanical properties of the metal in uniaxial elongation. Crack formation stress does not depend on the elastic energy storage. The development of cracks decreases with a greater elastic-energy storage. As regards the possibility of crack formation and development in a system with a higher elastic energy storage, type 1602 steel alloyed with 0.05% V, is preferable to steel 1602 and to steel with 0.1% V. There are 6 references. T. Fedorova [Abstracter's note: Complete translation]

Card 1/1

The state of the s

## MAVROTSKIY, I.V.; KRIVENKO, L.V.

Effect of banded structure in structural steels on the anisotropy of their mechanical properties and the limit of celd brittleness.

Stal: 21 no. 4:350-354 Ap 161.

(MIRA 14:4)

1. Ukrainskiy mauchno-issledovatel skiy institut metallov. (Steel, Structural-Metallography) (Strength of materials)

5/032/61/027/007/006/012 B110/B203

18.8200

Tomenko, Yu. S., and Mavrotskiy, I. V.

TITLE:

AUTHORS:

Effect of the reserve in elastic energy on the magnitude of true tensile strength

PERIODICAL: Zavodskaya laboratoriya, v. 27, no. 7, 1961, 883-887

TEXT: It is known that the reserve in elastic energy and the flexibility of the loading device affect considerably the destruction kinetics. The authors studied the effect of the reserve in elastic energy on the magnitude S<sub>k</sub> of the true tensile strength in the loaded system. Since the deformation range is considered with dropping tensile strength of the sample (after P<sub>max</sub>), the results obtained should follow the laws of the unloaded system. The authors studied the steels (I) 16Γ2 PT (16G2 FT) developed at the Ukrainskiy nauchno-issledovatel kiy institut metallow (Ukrainian Scientific Research Institute of Metals) (0.10% C; 1.50% Mn; (Ukrainian Scientific Research Institute of Metals) (0.10% C; 1.50% Mn; 0.27% Si; 0.09% V; 0.025% Ti; 0.016% S; 0.020% P), and (II) 19 P (19G) (0.25% C; 0.99% Mn; 0.27% Si; 0.040% S; and 0.021% P) after rolling and mechanical Card 1/7

8/032/61/027/007/006/012

Effect of the reserve in elastic energy ... Bi10/B205

aging (10% elongation and 1-hr tempering at 250°C). For (I),  $\sigma$ T=50.9kg/mm<sup>2</sup>;  $\sigma$ B=70.8kg/mm<sup>2</sup>;  $\sigma$ 10=15.5%, and  $\sigma$ 10=44%; for (II),  $\sigma$ T=32.8kg/mm<sup>2</sup>;

OB=50kg/mm<sup>2</sup>; <sub>10</sub>=18.8%, and γ<sub>k</sub>=42.3%. Cylindrical octuple samples with 4.5 mm diameter were tested on an MM-4P (IM-4R) machine with different flexibility of the loading device (A) 1, (B) 5.5, and (C) 17.2mm/t. (A) resulted from the initial rigidity of the test machine, (B) and (C) were obtained by introduction of elastic elements. With great flexibility, the rupture load (Fig. 2, P<sub>k</sub>) could not be determined with ordinary inertion

machines due to the high deformation rate preceding rupture. An increase in the reserve of elastic energy effects an increase of the load  $P_{\chi}$  of the instantaneous beginning of destruction, as well as a decrease in concentrated deformation between  $P_{\chi}$  and  $P_{max}$ . For determining the true tensile strength, the absolute elongation  $\Delta l_{\chi}$  is plotted on the deformation

axis (Fig. 2). From here, a straight line is drawn parallel to the

Card 2/7

8/032/61/027/007/006/012

Effect of the reserve in elastic energy ... B110/B203

elastic deformation section, the intersection of which with the perpendicular of P gives the load P (Fig. 2). According to V. G. Ulegin (Ref. 5: Zavodskaya laboratoriya, XXV, 10 (1959)), Sk increases linearly with increasing reserve of elastic energy, which is explained by a delayed retrogression of the load toward P. T. K. Zilova et al. (Zavodskaya laboratoriya, XXV, 1, (1959)) showed that retrogression of the outer load is the slower, the higher the flexibility and the reserve in elastic energy of the system, and the lower the plasticity of the metal. A slower decrease of the outer load as compared with the load on the sample was found oscilloscopically. This difference grows with time up to destruction. With the maximum accumulated reserve in elastic energy, A\_=2-3 kgm, at the end points of the oscillogram, it is 5-15 kg, with A =10-12 kgm, it is 90-100 kg. In this connection,  $P_x$  tends toward  $P_{max}$ , but theoretically it never attains it. Now, the effect of the reserve in elastic energy on the total course of the curve for true tensile strength was to be established. For calculating the sample cross section

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Effect of the reserve in elastic energy ... B110/B203

Card 4/7

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Effect of the reserve in elastic energy .. B110/B203

section measurement. The curvature begins with increasing reserve in elastic energy. This can only be explained by an increase in the deformation rate in the section of concentrated deformation after point P. The increase, in turn, is connected with the delayed retrogression of the outer load(after Pmax) and the increase of the reserve in elastic energy. There are 6 figures and 6 Soviet-ploc-references

ASSOCIATION: Ukrainskiy nauchno-issledovatel'skiy institut metallov (Ukrainian Scientific Research Institute of Metals).

Fig. 2. Elongation diagram with a yieldingness Y of the loading system of 17.2 mm/t. Legend:  $A_1$ =deformation work in the section between maximum load and beginning of "instantaneous" destruction  $(P_X)$ . (1) deformation, (2) load.

(1) Depopreus FIG2

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S/032/61/027/012/011/015 B104/B102

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Navrotskiy, I. V., and Tomenko Yu. S.

AUTHORS:

Influence of the strain gradient on tensile strength in

brittleness tests

PERIODICAL: Zavodskaya laboratoriya, v. 27, no. 12, 1961, 1520 - 1522

TEXT: The mean and actual strains in samples of varying diameter occurring in brittleness tests, were studied. (73(St. 3) steel samples were cooled with liquid oxygen before the test. The hot junctions of two thermocouples were placed in the incision of the samples, and strain gauges were fixed parallel to the horizontal axis, at distances of 2 mm. During the test, strains were recorded by an MNO2(MPO-2) oscilloscope. The tests were carried out with a 200-t press at -70°C. It is inferred from graphs of the results that the decrease in the mean tensile strengths is connected with an increase in the sample diameter and with a variation in the strain gradient. For a sample diameter between 175 and 1000 mm tensile stress is between 44 and 11 kg/mm<sup>2</sup>. This is attributed to the

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21398 \$/032/61/027/012/011/015 B104/B102

Influence of the strain gradient ...

increase in strain gradient with increasing sample diameter. The tensile stress of 11 kg/mm<sup>2</sup> obtained in brittleness tests is much lower than the creep strength, and is close to the value obtained for previously cracked samples. Strain around the incision was independent of the sample diameter and, consequently, of the strain gradient. F. Fili et al. (Sb. "IV Mezhdunarodnyy neftyanoy kongress" (IV International Petroleum Congress), v. VIII, p. 66. Gostekhizdat (1956)) is mentioned. There are 4 figures and 8 references: 4 Soviet and 4 non-Soviet. The three references to English-language publications read as follows: A. B. Bagsan Welding J., v. 28, no. 10, p. 484 - S (1949); H. E. Boodberg, H. E. Davis, E. R. Parker, G. E. Troxell. Welding J., v. 27, no. 4, p. 186 - S (1948). N. A. Kahn, E. A. Imbembo. Welding J., v. 27, no. 4, p. 169 - S (1948).

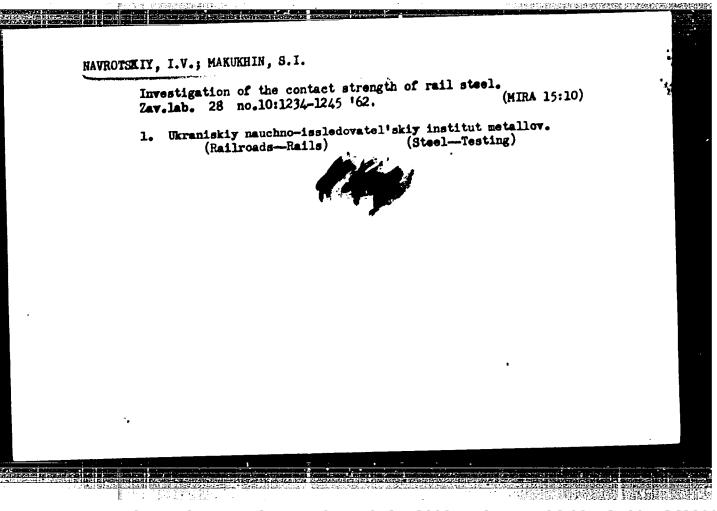
ASSOCIATION: Ukrainskiy institut metallov (Ukrainian Institute of Metals)

Card 2/2

MAKUKHIN, S.I.; NAVROTSKIY, I.V.; KAZARNOVSKIY, D.S.

Investigating the contact strength of steel for railroad rails.
Stal' 22 no.9:838-342 S '62. (MIRA 15:11)

1. Ukrainskiy nauchno-issledovatel'skiy institut metallov.
(Railroads--Rails--Testing)



S/032/63/029/001/020/022 B101/B186

AUTHORS:

Navrotskiy, I. V., and Tomenko, Yu. S.

TITLE:

Effect of the margin of energy on the destruction of steels having different plasticity in impact tearing tests

PERIODICAL: Zavodskaya laboratoriya, v. 29, no. 1, 1963, 87 - 90

TEXT: It is concluded from a paper by T. K. Zilova et al. (Zavodskaya laboratoriya, 25, 1, 1959, 76) that metals of high plasticity show a greater rate of deformation under the same overload than those which have greater rate of deformation under the same overload than those which have low plasticity. It may therefore happen that the destruction time of a loss plastic metal. With great margins of elastic destruction time of a less plastic metal. With great margins of elastic energy, in a series of steel types the sequence of destruction times may energy, in a series of steel types the sequence of destruction times may energy, in a series of steel types the sequence of destruction times may energy, in a series of steel types the sequence of destruction times may energy, in a series of steel types the sequence of destruction times may energy, and different this problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem by making impact tearing tests with a drop weight on cylindrithis problem.

5/052/65/029/001/020/022 B101/B186

Effect of the margin of energy on ...

approach the same value for all specimens, namely about 200 kgm and 3APPROVED FOR RELEASE: Monday July 15 2000 strect Property 100513R00113 plastic steels at high deformation rates. If the test bars were notched, the margin of energy at which steels of different plasticity had the same destruction time decreased to 20-40 kgm. A greater margin of energy increases considerably the sensitivity of strength to notching but does not affect the sensitivity to deformation. There are 5 figures.

ASSOCIATION: Ukrainskiy nauchno-issledovatel'skiy institut metallov (Ukrainian Scientific Research Institute of Metals)

NAVROTSKIY, I.V.; HAGUZIN, V.I.; TOMENKO Yu.S.

Effect of certain factors on the impact strength of various types of specimens. Zav. 1ab. 30 no.1:81-85 '64. (MIRA 17:9)

1. Ukrainskiy nauchno-issledovatel skiy institut motallov.

SANDLER, N.I.; GUREVICH A.B.; NAVROTSKIY, I.V.; YUMASH, V.M.; TURUBINER, L.M.; KIRZHNER, O.M.

Phase distribution of vanadium, tangsten, and niob to in low-alloy steels. Shor. trud. "NIIM no.91349-356" (...
(MIRA 18:1)

EFF(n)-2/mon(n) (min/h) (min/h) (min/h) (min/h) (min/h) 5/0277/65/000/601/0015/0015 ACCESSION MR: AR5008956 counce: Ref. zh. Mashinostroltel'nyvo materialy, konstruktsii i raschet detaley mashin, Otd. vyp., Ats. 1.49.53 AUFUOR: Mavrotskiy, I. V.; Tomenko, Yu. S.; Kurmanov, M. I. THE effect of minor admixtures of  $\frac{V}{2}$ ,  $\frac{H}{2}$  and  $\frac{Nb}{2}$  on the structural strength annuanese steel CITED BOURCE: Sb. tr. Ukr. n.-i. in-t metallov, vyp. 9, 1964, 357-376 KOFIG EAGS: manganese steel, steel vanadium alloying, tungsten alloying nichium alloying, steel structural strength, manganese content TRANSLATION: The following mechanical characteristics were selected as factors governing the structural strength of the steel: forack formation lead Pcr; load corresponding to tensile strength - Pmax; tensile sensitivity to stress concentration; time to failure; and strain sensitivity to stress concentration. V, W and Mb had a beneficial effect on the structural strength only in terms of an improved deformation resistance. Sensitivity to stress concentration and the tendercy to cold brittleness depended on the content of the alloying element and the content of Mn. Alloying of a steel with a high Mn content by adding

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L 45059-65	The second of th	o.	
ACCESSION NN: AR5008956	steel by adding 0.55% V, p	roduces the best	
o.29% Nh, of a low Mn centent structural properties for mat properties in materials with manganess steel with 0.08% Nh	ortain wave v is go are obta	dred by alloying high	
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1.41333-65 ENT(m)/EWP(w)/EFF(n)-2/EWA(d)/EPM/T/EWP(z)/EWP(z)/EWP(b)/EWA(c)

1JP(c) ID/JG

ACCESSION NR: AR5000593 S/0137/64/000/008/T044/I044

SOURCE: Ref. zh. Metaliurgiya. Sv. t., Abs. 81286

AUTHOR: Mavrotskiy, I. V.; Sandler, N. I.; Kurmanov, K. I.

WITER: The nature of hardening of low alloy manganese steels by rangelum, niobium and tungsten

CIVED SOUNCE: Su. tr. Ukr. n. i in-t metallov, vywp. 9, 1964,

377-393

TOPIO TAGS: vanadium containing alloy, miobium containing alloy, Mungsten containing alloy, manganese bentaining alloy, manganese steel, metal hardening, steel hardening.

TRANSLATION: The physical nature of the hardening of manganese steel alloyed with small additions of vanadium, niobium and tungsten as been investigated. For study of the effect of manganese on the steel hardening of low alloy steel, we grape of melts were made with internal centents of the alloying elements, but with a different content of manganese; high (1.3-1.5%) and low (1.5-0.7%). In

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addition, melts were made with different manganese contents, but without supplementary alloying. A study was made of the mechanical supplements of the steel, the metallographic attracture, the change in which of K-ray interference lines, and the phase limited from fragmentation our of the process of medical translations of the following eachs: I make district the change in the solution lattice (with alloying by small additions of variation, colution lattice (with alloying by small additions of variation, colutions and alloying with turnster), 3 the effect of the carbide from with microstresses and the nature of the distribution of the saletying atoms in the solid solution lattice (on alloying with microstresses and the nature of the distribution of the saletying atoms in the solid solution lattice (on alloying with microstresses titles.

SUB CODN: M4 ENCL: 00

BAGUTIN, V.I.; MAVECTSKIY, I.V.

Mathod for determining the critical temperature of brittleness in impact strength tests. Zav. lav. 31 no.1:100-103 '65. (MRA 18:3)

1. Ukrainskiy nauchno-issledovatel'skiy institut metallov.

MAYROTSHIY, N.V., mekhanik

Performance of turbobits on heavy clay muds. Meftianik
5 no.5:14-15 My \*60.

1. Shebelinekaya kontora bureniya tresta Kharburneftegaz.
(Aurbodrills)

14(6)

SOV/98-59-6-2/20

AUTHORS:

Strokov, G.I., and Navrotskiy, P.A., Engineers

TITLE:

A Wide-Seam Cyclopic Stonework

PERIODICAL:

Gidrotekhricheskoye stroitel'stvo, 1959, Nr 6, pp 9

12 (USSR)

ABSTRACT:

The method of wide-seam cyclopic stonework was proposed by the authors in collaboration with engineers I.T. Novikov, V.Ya. Sherskov and N.V. Khvoshchinskiy. and was tried out during the construction of the left bank pier of the Kremenchug GES from July to November 1958. Large stone blocks (volume 2 cu m and more)

were cut out from a near-by quarry. The already cleared foundation was covered by a layer of vibrated concrete, 20 to 30 cm thick, and the rocks were then placed on it by cranes at 20 cm intervals, 20 cm from the edge of the lining. Intervals between the rocks are necessary so that the concrete which fills the intervals or seams can be thoroughly vibrated. The

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first layer thus obtained is again covered with con

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sov/98-59-6-2/20

A Wide-Seam Cyclopic Stonework

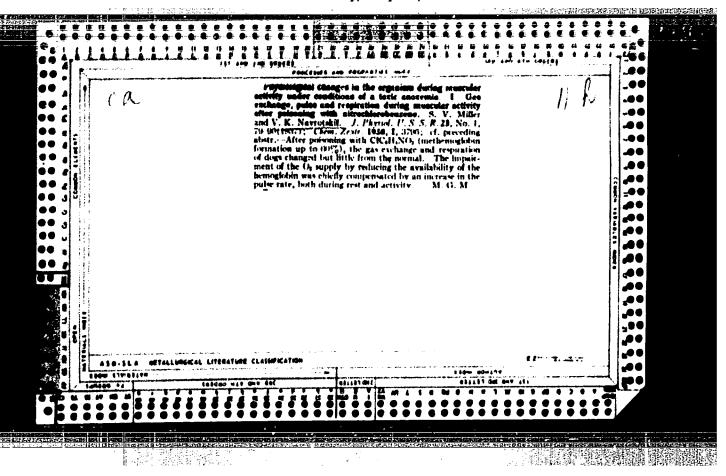
crete, and the operation is continued until the needed height is reached. The authors describe different tests made to ascertain the strength of such structures. All operations were timed, and it was found that considerable savings in material, time and money could be achieved, provided, a sufficient number of blocks are prepared in advance. There are 4 photographs.

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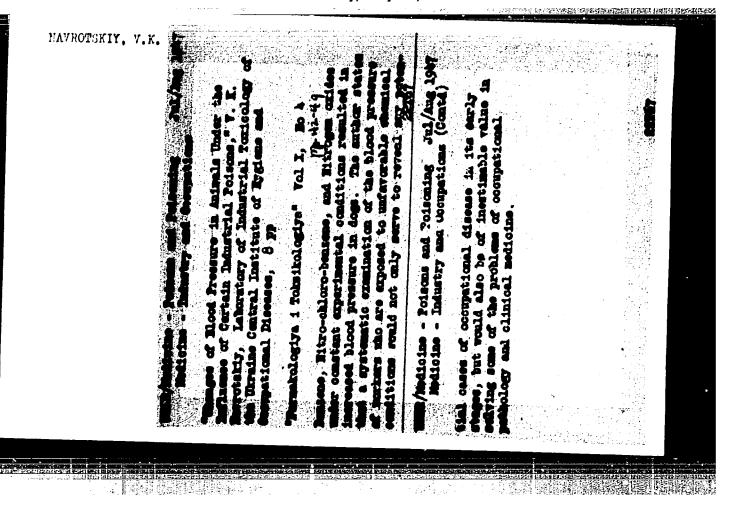
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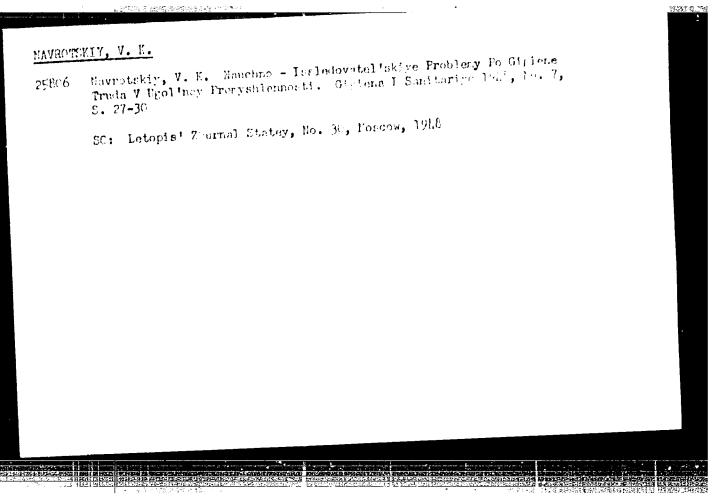
FANADIADI, A.D., kand. sel'khoz. nauk; VOLOVSKIY, S.P., kand. sel'khoz. nauk; NAVROTSKIY, S.K., kand. sel'khoz. nauk; PANADIADI, Ye.A., inzh.; SPIRIDONOV, A.L., kand. sel'khoz. nauk; TIMOFEYEV, A.F., kand. sel'khoz. nauk; LAPIDOVSKIY, K.I., red.

[Agricultural melioration] Sel'skokhoziaistvennaia melioratsiia. Moskva, Kolos, 1965. 502 p. (MIRA 18:7)



14 1.720 NAVACTZKIY, V. K. May/Jun 1947 USER/Medicine - Histology Chemistry - Aniline "The Distribution of Aniline in the Animal Tissues," V. K. Navrotzkiy, I. M. Orlik, 3 pp "Fermakol i Toksikol" Vol X, No 3 Results of a study of the distribution of aniline as representative of a large group of amino and nitro derivatives of benzol, injected into the femoral vein of dogs. It is concluded, among other points, that the aniline content in the blood at a later stage of the poisoning is an average index of the aniline content in the whole organism. 14726





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NAVROTSKIY, V.A.

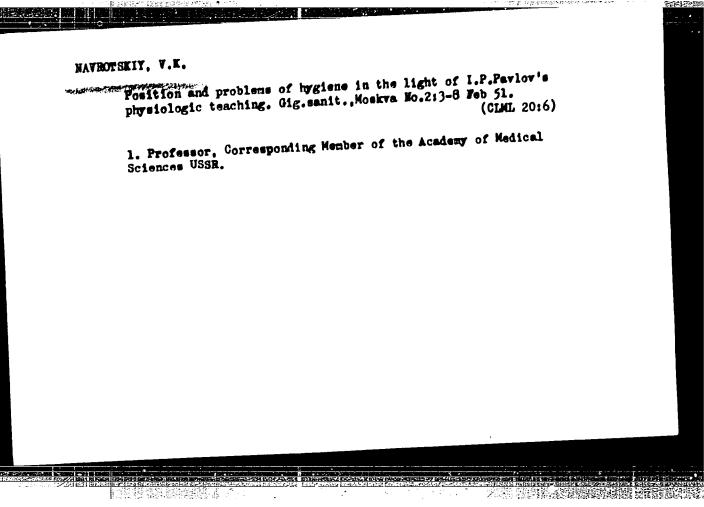
37551 Voprosy gigiyeny truda v ugol'noypromyshlennosti v poslevoyennoye vremya,
V Shixii veesoyuz. S'yezd gigiyenistov, epidemiolo, ov, mikrobiologov i infektsi
Stov. T.1.M., 1949, 154-29

SO: Letopis'Zhurnal'nykh statey, Vol. 37,1949

NAVROTSKIY, V. K.

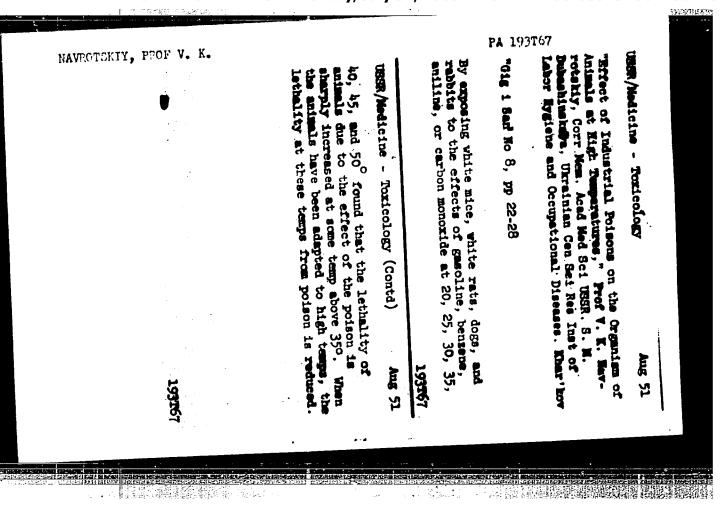
Navrotskiy, V. K. "The basic tasks of labor hy, iene in the industry of the Ukraine in the immediate future," Vracheb. delo, 1343, No. 3, paragraphs 253-36.

SO: U-3736, 21 May 53, (Letopis 'Zhurnal 'nykh Statey, No. 18, 1943).



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CIA-RDP86-00513R0011362200

## HAVROTSKIY, V.K.

The area of industrial toxicology as an aspect of Pavlov neurology. Gigiena i Sanit. '53. No.4, 3-11. (KLRA 6:4) (CA 47 no.21:11536 '53)

A detailed discussion on the varied effects of commercial poisons on the central nervous system. Describes experiments on snimals. Lists several laboratories concerned with toxicology.

Translation M-751, 30 aug 55

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